



Standard Test Method for Nondestructive Assay of Plutonium in Scrap and Waste by Passive Neutron Coincidence Counting¹

This standard is issued under the fixed designation C 1207; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

1. Scope

1.1 This test method describes the nondestructive assay of scrap or waste for plutonium content using passive thermal-neutron coincidence counting. This test method provides rapid results and can be applied to a variety of carefully sorted materials in containers as large as 208-L drums. The test method applies to measurements of ^{238}Pu , ^{240}Pu , and ^{242}Pu and has been used to assay items whose total plutonium content ranges from 0.01 to 6000 g (1).²

1.2 This test method requires knowledge of the relative abundances of the plutonium isotopes to determine the total plutonium mass.

1.3 This test method may not be applicable to the assay of scrap or waste containing other spontaneously fissioning nuclides.

1.3.1 This test method may give biased results for measurements of containers that include large amounts of hydrogenous materials.

1.3.2 The techniques described in this test method have been applied to materials other than scrap and waste (2, 3).

1.4 This test method assumes the use of shift-register-based coincidence technology (4).

1.5 Several other techniques that are related to passive neutron coincidence counting exist. These include neutron multiplicity counting (5,6), add-a-source analysis (7), and cosmic-ray rejection (8). Discussions of these techniques are not included in this method.

1.6 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

¹ This practice is under the jurisdiction of ASTM Committee C26 on Nuclear Fuel Cycle and is the direct responsibility of Subcommittee C26.10 on Nondestructive Assay.

Current edition approved Feb. 10, 2003. Published March 2003. Originally approved in 1991. Last previous edition approved in 1997 as C 1207-97.

² The boldface numbers in parentheses refer to the list of references at the end of this test method.

2. Referenced Documents

2.1 ASTM Standards:

C 859 Terminology Relating to Nuclear Materials³

C 986 Guide for Developing Training Programs in the Nuclear Fuel Cycle³

C 1009 Guide for Establishing a Quality Assurance Program for Analytical Chemistry Laboratories Within the Nuclear Industry³

C 1030 Test Method for Determination of Plutonium Isotopic Composition by Gamma-Ray Spectrometry³

C 1068 Guide for Qualification of Measurement Methods by a Laboratory Within the Nuclear Industry³

C 1128 Guide for the Preparation of Working Reference Materials for Use in the Analysis of Nuclear Fuel Cycle Materials³

C 1133 Standard Test Method for NDA of Special Nuclear Material in Low Density Scrap and Waste by Segmented Passive Gamma-Ray Scanning³

C 1156 Guide for Establishing Calibration for a Measurement Method Used to Analyze Cycle Materials³

C 1210 Guide for Establishing a Measurement System Quality Control Program for Analytical Chemistry Laboratories within the Nuclear Industry³

C 1215 Guide for Preparing and Interpreting Precision and Bias Statements in Test Method Standards Used in the Nuclear Industry³

C 1500 Test Method for Nondestructive Assay of Plutonium by Passive Neutron Multiplicity Counting³

2.2 ANSI Standards:⁴

ANSI 15.20 Guide to Calibrating Nondestructive Assay Systems

ANSI 15.35 Guide to Preparing Calibration Materials for NDA Systems that Count Passive Gamma-Rays

ANSI 15.36 Nondestructive Assay Measurement Control and Assurance

³ Annual Book of ASTM Standards, Vol 12.01.

⁴ Available from American National Standards Institute, 11 W. 42nd St., 13th Floor, New York, NY 10036.

3. Terminology

The following definitions are needed in addition to those presented in ASTM C 859.

3.1 Definitions:

3.1.1 (α, n) reactions—occur when energetic alpha particles collide with low atomic number nuclei, such as O, F, or Mg, producing single neutrons.

3.1.2 coincidence Gate Length—the time interval following the detection of a neutron during which additional neutrons are considered to be in coincidence with the original neutron.

3.1.3 coincident neutrons—two or more neutrons emitted simultaneously from a single event, such as from a nucleus during fission.

3.1.4 Die-away time—the average life time of the neutron population as measured from the time of emission to detection, escape, or absorption. The average life time is the time required for the neutron population to decrease by a factor of $1/e$. It is a function of several parameters including chamber design, detector design, assay item characteristics, and neutron energy.

3.1.5 item—an item refers to the entire scrap or waste container being measured and its contents.

3.1.6 matrix—the material which comprises the bulk of the item, except for the special nuclear material and the container. This is the material in which the special nuclear material is embedded.

3.1.6.1 benign matrix—a matrix that has negligible effects on neutron transport. A benign matrix includes very little neutron moderator.

3.1.6.2 matrix-specific calibration—uses a calibration matrix similar to the matrix to be measured. No matrix correction factors are used. This calibration is generally not appropriate for other matrices.

3.1.7 neutron absorbers—materials which have relatively large thermal-neutron absorption cross sections. Absorbers

with the largest cross sections are commonly known as neutron poisons. Some examples are lithium, boron, cadmium, and gadolinium.

3.1.8 neutron moderators—materials which slow down neutrons. Materials containing large amounts of low atomic weight materials, e.g. hydrogen are highly moderating.

3.1.9 passive neutron coincidence counting—a technique used to measure the rate of coincident neutron emission in the assay item. The terminology used in this test method refers specifically to shift-register electronics (9, 10). Fig. 1 shows the probability of detecting a neutron as a function of time and illustrates the time intervals discussed.

3.1.9.1 Shift-register-based coincidence circuit—an electronic circuit for determining totals τ , reals plus accidentals ($r + a$), and accidentals (a) in a selected count time t (9, 10). Shift register-based circuitry was developed to reduce dead times in thermal neutron coincidence counters. This technique permits improved measurement precision and operation at higher count rate ($\geq 100\text{kHz}$).

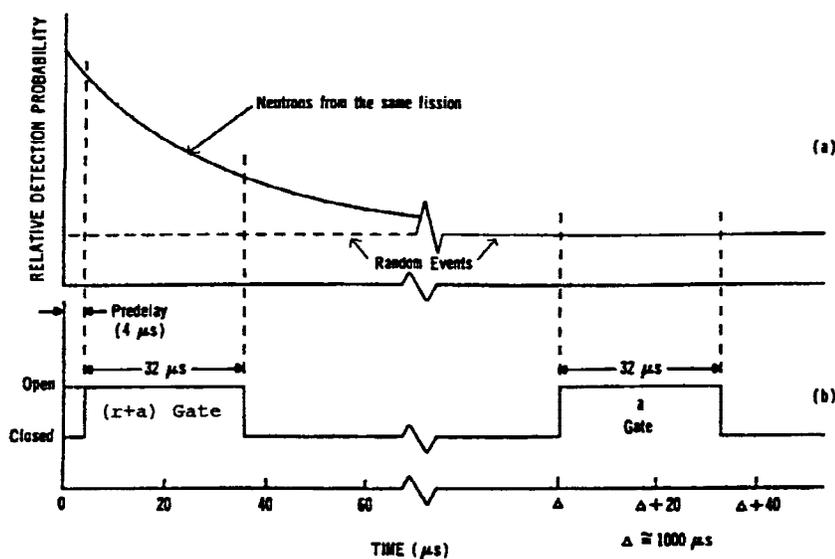
3.1.9.2 totals τ —the total number of neutrons detected during the count time. This is a measured quantity.

3.1.9.3 reals plus accidents, ($r + a$)—the number of neutrons detected in the ($r + a$) gate period (Fig. 1) following the initial detection of each neutron. This is a measured quantity during the count time (4, 9).

3.1.9.4 accidentals, (a)—the number of neutrons detected in the (a) gate period (Fig. 1) following the initial detection of each neutron during the selected count time t . This is a measured quantity (4, 9).

3.1.9.5 Reals, (r)—This quantity is the difference between the ($r+a$) and (a) quantities (4,9). It is proportional to the number of fissions in the sample.

3.1.10 Neutron multiplication—Multiplication takes place when a neutron interaction yields more than one neutron as a



NOTE 1—Curve (a) is a simplified probability distribution showing the approximately exponential decay, as a function of time, for detecting a second neutron from a single fission event. The probability for detecting a random neutron is constant with time. Typical coincidence timing parameters are shown in (b).

FIG. 1 Probability of Detection as a Function of Time

product. Induced fission is the primary mechanism for neutron multiplication, however (n,2n) interactions are also multiplication events.

3.1.11 *Poisson assumption*—For passive neutron coincidence measurements, it is assumed that the net counts in a fixed period of time follow a Poisson distribution. This assumption can be verified by comparing the observed standard deviation of a series of measurements on an item with the square root of the average number of counts. If the Poisson assumption is correct, these numbers should be equal within random error.

3.1.12 *Precision*—The precision of a measurement is taken to be the standard deviation or (percent) relative standard deviation of a series of measurements taken on the same item under essentially the same conditions.

3.1.13 *Pre-delay*—the coincidence circuit has a pre-delay immediately after a neutron has been detected to allow the amplifiers to recover and prepare to detect subsequent neutrons. This principle is shown in Fig. 1.

²⁴⁰Pu *effective mass*, m_{eff} —is the mass of ²⁴⁰Pu that would produce the same coincident neutron response in the instrument as the assay item. It is correlated to the quantity of even mass isotopes of plutonium in the assay item (11).

3.1.15 *transuranic waste (TRU waste)*—as defined in DOE Order 5820.2 (12), transuranic waste is radioactive waste containing alpha-emitting isotopes with atomic number greater than 92 and half-life greater than 20 years, and with activity concentrations greater than 100 nCi per gram of waste at the time of the measurement.

4. Summary of Test Method

4.1 The even mass isotopes of plutonium fission spontaneously. On the average, two or more neutrons are emitted per fission event. The number of these coincident neutrons detected by the instrument is correlated to the quantity of even mass isotopes of plutonium in the assay item, m_{eff} . The total plutonium mass is determined from the known plutonium isotopic ratios and the measured quantity of even mass isotopes.

4.2 The shift register technology is intended to correct for the effects of *accidental* neutron coincidences.

4.3 Other factors which may affect the assay are neutron multiplication and matrix components with large (α , n) reaction rates, neutron absorbers, or moderators. Corrections for these effects are often not possible from the measurement data alone, consequently assay items are sorted into material categories or additional information is used to obtain the best assay result.

4.4 Corrections are typically made for electronic deadtime and neutron background.

4.5 Calibrations are based on measurements of well documented and appropriate reference materials.

4.6 This method includes measurement control tests to verify reliable and stable performance of the instrument.

5. Significance and Use

5.1 This test method is useful for determining the plutonium content of scrap and waste in containers as large as 208-L (55-gal) drums. Total plutonium content ranges from 10 mg to 6 kg (1). The upper limit may be restricted to smaller mass

values depending on specific matrix, calibration material, criticality safety, or counting equipment considerations.

5.2 This test method is applicable for U.S. Department of Energy shipper/receiver confirmatory measurements (13), nuclear material diversion detection, and International Atomic Energy Agency attributes measurements (14).

5.3 This test method should be used in conjunction with a scrap and waste management plan that segregates scrap and waste assay items into material categories according to some or all of the following criteria: bulk density, the chemical forms of the plutonium and the matrix, americium to plutonium isotopic ratio, and hydrogen content. Packaging for each category should be uniform with respect to size, shape, and composition of the container. Each material category will require calibration standards and may have different plutonium mass limits.

5.4 Bias in passive neutron coincidence measurements is related to item size and density, the homogeneity and composition of the matrix, and the quantity and distribution of the nuclear material. The precision of the measurement results is related to the quantity of nuclear material, the (α ,n) reaction rate, and the count time of the measurement.

5.4.1 For both benign matrix and matrix specific measurements, the method assumes the calibration reference materials match the items to be measured with respect to the homogeneity and composition of the matrix, the neutron moderator and absorber content, and the quantity of nuclear material, to the extent they affect the measurement.

5.4.2 Measurements of smaller containers containing scrap and waste are generally more accurate than measurements of 208-L (55-gal) drums.

5.4.3 It is recommended that measurements be made on items with homogeneous contents. Heterogeneity in the distribution of nuclear material, neutron moderators, and neutron absorbers have the potential to cause biased results.

5.5 The coincident neutron production rates measured by this test method are proportional to the mass of the even number isotopes of plutonium. If the relative abundances of these isotopes are not accurately known, biases in the total plutonium assay value will result.

5.6 A typical count time is 1000 seconds.

5.7 Reliable results from the application of this method require training of the personnel who package the scrap and waste prior to measurement and of personnel who perform the measurements. Training guidance is available from ANSI 15.20, ASTM C 1009, ASTM C 986, and ASTM C 1068.

6. Interferences

6.1 Conditions affecting measurement uncertainty include neutron background, moderators, multiplication, large (α , n) rates, absorbers, matrix and nuclear material heterogeneity, and other sources of coincident neutrons. It is usually not possible to detect these problems or to calculate corrections for these effects from the measurement data alone. Consequently, assay items are sorted into material categories defined on the basis of these effects.

6.2 Neutron background levels from external sources should be kept as low and as constant as practical. Corrections can be

made for the effects of high-neutron background levels, but these will adversely affect measurement precision and detection limits.

6.3 Neutron moderation by low atomic mass materials will not only increase thermal-neutron absorption effects, but will also increase multiplication effects. Consequently, the measured neutron rates may be either smaller or larger than those for a nonmoderating matrix. Hydrogenous matrices contribute the most to this effect (15).

6.4 Both spontaneous and induced fissions produce coincident neutrons. The instrument, however, cannot distinguish between them. Three factors that strongly affect the degree of multiplication are the mass of fissile material, its density, and its geometry. Increases in mass that are not accompanied by changes in either density or geometry will result in predictable multiplication increases that can be incorporated into the calibration function. Localized increases in nuclear material density and/or changes in the geometry are likely to cause unknown changes in multiplication and measurement bias.

6.5 Neutrons from (α , n) reactions are an interference (bias) source if they induce multiplication effects. In addition, (α , n) neutrons can increase the accidental rate thereby affecting the statistical precision of the assay.

6.6 Biases may result from non-uniformity in the source distribution and heterogeneity in the matrix distribution.

6.7 Other spontaneous fission nuclides (for example, curium or californium) will increase the coincident neutron count rates, causing an overestimation of the plutonium content.

6.8 Cosmic rays, which are difficult to shield against, can produce coincident neutrons. Cosmic ray effects become larger for small quantities of plutonium in the presence of large quantities of high atomic number materials, for example, iron or lead (see 12.5).

7. Apparatus

7.1 *Counting Assembly*—See Fig. 2.

7.1.1 The apparatus used in this test method can be obtained commercially. Specific applications may require customized design. The neutron detectors are usually ^3He proportional counters embedded in polyethylene. The detection efficiency

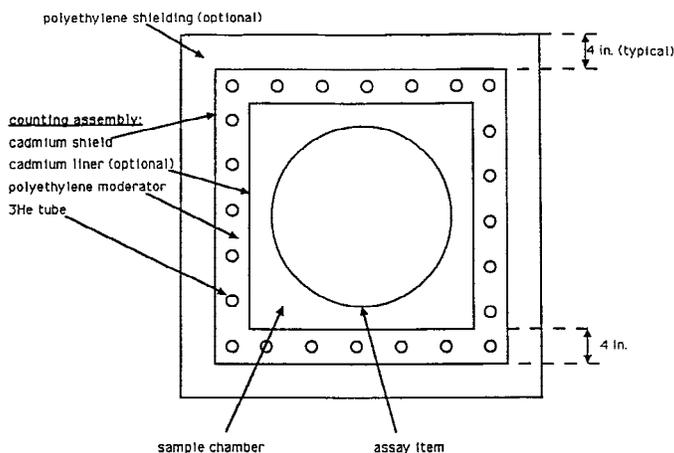


FIG. 2 A Cross-section View of a Typical Thermal-Neutron Coincidence Counter

for neutrons of fission energy should be at least 15 %. Larger detection efficiencies provide better precision and lower detection limits for a given count time. Ideally, the counter detection efficiency should vary less than 10 % over the item volume.

7.1.2 Reproducible positioning of the item in the chamber is important for obtaining the best accuracy. This counting geometry should be maintained for the measurement of all reference materials and assay items. (See 11.7.)

7.1.3 A 0.4 mm to 1mm thick cadmium liner (16) is often installed on the inside surfaces of the counting chamber surrounding the assay item. This liner will decrease multiplication inside the item and decrease the effects of neutron absorbers inside the item. The liner will also decrease neutron detection efficiency due to absorption of thermalized neutrons and may increase the cosmic ray spallation background.

7.2 *Shielding*—The detector assembly is often surrounded by cadmium and an additional layer of hydrogenous material (see Fig. 2). Four inches of polyethylene can reduce the neutron background in the sample chamber by approximately a factor of 10 (17).

7.3 *Electronics*—High-count-rate nuclear electronics provide a standard logic pulse from the proportional counters. These pulses are processed by the shift-register coincidence technology.

7.4 Data acquisition and reduction can be facilitated by interfacing the instrument to a computer.

8. Hazards

8.1 *Safety Hazards*—Consult qualified professionals as needed.

8.1.1 Precautions should be taken to prevent inhalation, ingestion, or the spread of plutonium contamination during waste or scrap handling operations. All containers should be surveyed on a regular basis with an appropriate monitoring device to verify their continued integrity.

8.1.2 Precautions should be taken to minimize personnel exposure to radiation.

8.1.3 Precautions should be taken regarding nuclear criticality, especially of unknown items. The measurement chamber approximates a reflecting geometry for fast neutrons. The assumption that waste is not of criticality concern is not recommended.

8.1.4 Counting chambers may contain a cadmium liner. Precautions should be taken to prevent the inhalation or ingestion of cadmium. It is a heavy metal poison. Cadmium shielding should be covered with nontoxic materials.

8.1.5 Precautions should be taken to avoid contact with high voltage. The ^3He tubes require low current, high voltage, power supplies.

8.1.6 The weight of the instrument may exceed facility floor loading capacities. Check for adequate floor loading capacity before installation.

8.2 *Technical Hazards:*

8.2.1 Locate the instrument in an area of low-neutron background. Prohibit the movement of radioactive material in the vicinity of the instrument while a measurement is in progress.

8.2.2 Utilizing a measurement result outside of the calibration range should be carefully evaluated and, in general, is not recommended.

8.2.3 Utilizing a measurement result based on a calibration for a different material category should be carefully evaluated and, in general, is not recommended.

9. Instrument Preparation and Calibration

NOTE 1—Instrument preparation, determination of material categories, and calibration of passive neutron coincidence counters is discussed in the section below. Many details of these operations are site specific, depend on the matrix categories and nuclear materials to be measured, and should be evaluated by experts. Additional sources of information are ASTM C 1009, C 1068, C 1128, C 1156, C 1210, and C 1215; ANSI 15.20, 15.35, and 15.36.

9.1 Initial Preparation of Apparatus:

9.1.1 Locate the instrument in an area with the lowest practical neutron background. Prohibit the movement of radioactive material in the vicinity of the instrument while a measurement is in progress.

9.1.2 Perform the initial setup recommended by the system manufacturer.

9.1.3 If the die-away time and dead-time correction coefficients were not supplied by the manufacturer, determine them. Consult an appropriate text on radiation detectors (18) or the manufacturer if assistance is needed.

9.1.4 If it is a user adjustable feature, set the gate length. The optimum gate length for a wide range of count rates is 1.257 times the die-away time (19). Low count rate applications sometimes benefit from longer gate lengths. Changing the gate length alters all calibrations. Whenever the gate length is changed, the instrument must be recalibrated.

9.1.5 If it is a user adjustable feature, place the necessary cadmium liners in the assay chamber. Very low gram quantity applications benefit from having no cadmium liner. Separate calibrations are required for each cadmium liner configuration.

9.1.6 Use a stable neutron source and refer to vendor's manuals to verify that the electronics are stable and operating properly.

9.1.6.1 Place a source of coincident neutrons, for example, ^{252}Cf with an emission rate of $\sim 4 \times 10^4$ neutron/s, in the center of the counting chamber. Determine the totals (T), reals (R), and accidentals (A) neutron count rates from the measured quantities.

$$A = a/t, \quad (1)$$

$$A_{calc} = T^2 \times \text{gate length}, \quad (2)$$

$$R = [(r + a) - a]/t \quad (3)$$

where:

$$T = \text{totals rate} = \tau/t. \quad (4)$$

A necessary but not sufficient indication of proper electronics operation is agreement between A_{calc} and A within counting statistics. This test is termed the Accidentals/Totals test.

9.1.6.2 Leaving the ^{252}Cf neutron source inside the assay chamber, place a source of random neutrons, for example, americium-lithium with an emission rate of $\sim 4 \times 10^4$ neutrons/s, in, or near, the counting chamber. Determine the

reals rates from the measured quantities for ^{252}Cf with and without the random neutron source. The reals rates should agree to within counting statistics for the two measurements (see 11.1).

9.1.6.3 Use these measurements as part of the measurement control data described in 10.1.

9.2 Determination of Material Categories for Required Calibrations:

9.2.1 Use this test method in conjunction with a scrap and waste management plan that segregates scrap and waste materials into categories with respect to the characteristics discussed in 5.3, and Sections 6 and 12. Packaging for each category defined must be uniform. Each material category will require a set of representative reference materials.

9.2.2 The material categories are normally one of three classifications: oxide, metal, or salt.

9.2.3 The effectiveness of the scrap and waste management plan and the validity of the resulting calibrations are best evaluated by the R/T ratio check described in Appendix X1.

9.3 Preparation and Characterization of Reference Materials:

9.3.1 Reference materials should be as similar as possible to the assay items with respect to parameters such as size, shape, and composition which affect the measurement (see 5.3).

9.3.1.1 The plutonium mass loadings should span the range of loadings expected in the assay items and be adequate to define the shape of the calibration curve. Three to eight mass loadings are deemed suitable for each material category.

9.3.1.2 The reals-to-totals ratio, (R/T), may be used as an indicator to determine whether the neutron emission characteristics of the measured item matches the reference materials. Reasonable agreement between the R/T ratios for the reference materials and assay items (defined by a facility-dependent evaluation for each material category) suggests that the reference material is appropriate. See Appendix X1 for more information.

9.3.2 For waste measurements of small gram quantities of plutonium, dilute the plutonium used in the reference materials sufficiently to eliminate multiplication effects.

9.3.3 Certify the reference materials by a technique that has significantly smaller measurement uncertainty than that desired for the coincidence counter results.

9.3.4 Permanently record the following information for each reference material: packaging material(s), matrix, plutonium mass, m_{eff} , plutonium isotopic composition, and americium content with the date(s) measured.

9.4 Calibration Procedure—Use the following calibration procedure for each material category.

9.4.1 Calibration of a neutron coincidence counting instrument determines the relationship between the reals count rate (R) and the ^{240}Pu effective mass, m_{eff} .

9.4.2 Measure each reference material such that the measurement precision is 3 to 5 times better than that expected for assay items of similar plutonium mass. See Section 10.2 for counting procedures and Section 11 for required calculations.

9.4.3 Choice of calibration functions will depend on the characteristics of the material category as indicated below.

9.4.3.1 Measurements of small quantities of plutonium that exhibit no multiplication will normally show a linear relation of the form:

$$R = a_0 + a_1 m_{eff} \quad (5)$$

where a_1 and a_0 are coefficients determined by the fitting procedure.

9.4.3.2 Measurements of large quantities of plutonium of consistent chemical form and item geometry, will normally show a calibration function of the form:

$$R = a_0 + a_1 m_{eff} + a_2 (m_{eff})^2 \quad (6)$$

where:

a_0, a_1, a_2 = coefficients determined by the fitting procedure.

9.4.3.3 If the calibration is to be extended to total plutonium masses below 10 g, the calibration may produce less bias if a_0 is set to zero rather than fitted.

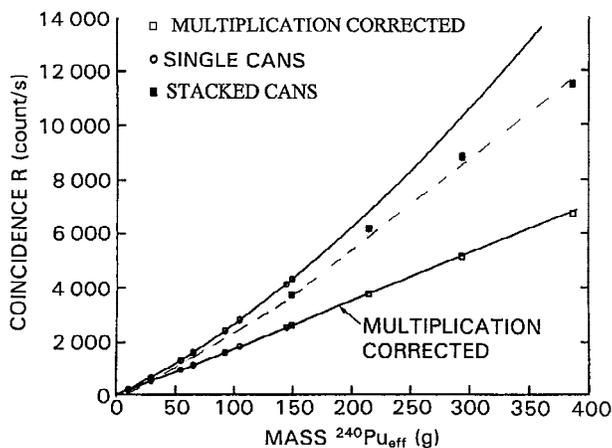
9.4.4 Record the allowed range of plutonium mass for the material category. The largest plutonium reference item typically places an upper limit on the assay range. Similarly, the lowest-valued plutonium reference item typically places a lower limit on the assay range. Utilizing a measurement result outside of the range of the calibration is not recommended.

9.4.5 Fig. 3 illustrates a problem that may occur when large plutonium mass items are simulated by stacking sample cans on top of each other. Because of geometric decoupling, self-multiplication is less than expected for a single can with the same high mass.

10. Procedure

NOTE 2—After calibration, the analytical procedure consists of measurements that demonstrate that the apparatus is calibrated and functioning properly (measurement control) and measurements of items with unknown plutonium content.

10.1 *Measurement Control*—The need for adjustment of the instrument can be determined by measurement control procedures (21). Frequent measurement of the coincidence rates of a



NOTE 1—Measured coincidence rate for two different measurement geometries (upper two curves) and multiplication corrected rate (bottom curve). Data for the curves was taken from Reference 20.

FIG. 3 Calibration Curves for Plutonium in a Neutron Coincidence Counter

reference material should be used to validate proper instrument operation. If instrument malfunction is suspected, perform all measurement control tests (Section 9.1.6) to provide data helpful to analyze the condition of the measurement system (Sections 10.1.1-10.1.4). Maintain measurement control charts to archive and monitor measurement control results and to make decisions about the need for calibration or maintenance (Reference ASTM C 1210). If measurement control indicates the instrument response has changed, determine the cause of the change. Then it will be clear whether to repair the instrument or repeat the calibration procedure, or both.

10.1.1 Perform periodic background counts before the measurement of assay items. Changes in the R and T values from historical values should be investigated (21).

10.1.2 Perform periodic counts of a well-characterized item or reference material to verify the long-term stability of the instrument. Typical practice is a daily check, if the instrument is used daily. For less frequent use, typical practice is to perform an instrument check before and after each period of use. Agreement of the measurement value with its reference value, within control limits, indicates proper operation of the instrument. Low results may indicate that a detector or detector bank is not functioning. High results may indicate electrical noise.

10.1.2.1 The item being used for the instrument check must provide a consistent coincidence signal. Suitable items are a ²⁵²Cf source corrected for decay, a reference material, or other stable source in which the material is fixed. Any characteristic which affects the coincidence neutron signal must not vary between measurements. Using a source in which the material is likely to change in some respect, such as bulk density, shape, or position of the material in the outer container, is not recommended.

10.1.3 Perform periodic replicate measurements of items to verify that the Poisson assumption is valid. This test might be done monthly or after each calibration. Statistical agreement between the standard deviation of the replicates and the uncertainty estimate based on counting statistics from each replicate indicates adequate stability of the instrument. Lack of agreement suggests background variations or electrical instabilities.

10.1.4 If measurement control criteria are passed, proceed to assays. If measurement control criteria fail, diagnose and correct the problem. Then proceed to setup, calibration, or repeat measurement control measurements.

10.2 Item Measurements:

10.2.1 If possible, center the assay item both vertically and horizontally in the counting chamber. This counting geometry should be maintained for all reference materials and assay items.

10.2.2 Count for the chosen count time.

10.2.3 When the count is complete, record, at a minimum, the assay item identifier τ , $r + a$, a , and the elapsed count time, t . For neutron coincidence counters under computer control, this information is recorded automatically.

10.2.4 Remove the assay item from the counting chamber.

10.2.5 Proceed to calculate the amount of plutonium present in the assay item.

10.2.6 The following diagnostic tests are recommended for each measurement.

10.2.6.1 The totals neutron count rate can be used to estimate the accidentals rate in the “accidentals/totals” test as shown in Sec 9.1.7.1. Lack of agreement within statistical uncertainty between the estimated and measured accidental count rates suggests a hardware failure in the coincidence circuitry or that the background neutron count rate changed significantly during the measurement.

10.2.6.2 Each measurement can be divided into several counting periods, and statistical tests can be performed that look for outliers in the individual counting periods (8). This “outlier” test reduces the effects of cosmic-ray background or of changing conditions during the measurement.

11. Calculation

NOTE 3—This section provides a summary of the calculations. The calculations are typically performed by the system software rather than by the operator. The vendor should provide assurance that the calculations are correctly implemented in the software. The calculations follow the same general approach whether the results are used for calibration, measurement control, or determining the plutonium content in an item.

11.1 Determine the reals coincidence rate, R (Eq 7).

$$R = [(r + a) - a]/t \quad (7)$$

11.1.1 Determine the totals rate:

$$T = \tau/t \quad (8)$$

11.1.2 Estimate the standard deviation of the coincidence rate for a single measurement:

$$\begin{aligned} \sigma_R &= 1.20w \frac{\sqrt{(r+a)+a}}{t} \\ &= 1.20 \sqrt{\frac{(R+2A)}{t}} \end{aligned} \quad (9)$$

The weighting factor w , approximately equal to 1.20, is a function of the detector parameters and the count rates, and is included because $r + a$ and a are correlated (4,22). The estimate of the standard deviation of the totals rate is:

$$\sigma_T = \frac{\sqrt{\tau}}{t} = \sqrt{\frac{T}{t}} \quad (10)$$

11.2 *Background Correction*—Subtract the corresponding background rate from the measured quantities.

$$R' = R - R_b \quad (11)$$

$$T' = T - T_b \quad (12)$$

where:

R_b = reals rate for an empty chamber and
 T_b = totals rate for an empty chamber.

11.3 *Dead-time Correction*—Samples with large quantities of plutonium or matrices with a large source of (α , n) neutrons can produce high count rates. It is important to make a correction for rate related counting losses (18). The corresponding corrected count rates, R_c and T_c are:

$$R_c = R' \exp(dT_c) \quad (13)$$

$$T_c = T' \exp(dT_c/4) \quad (14)$$

where:

d = dead-time coefficient = $c_1 + (C_2 10^{-6} T_c)$.

11.3.1 In these expressions, the quantity T_c in the exponent is often approximated by T' (2).

11.3.2 The manufacturer should supply the coefficients c_1 , c_2 with the delivery of the instrument. The coefficients depend on the instrument design.

11.3.3 Typical values for a system with six amplifier-discriminators are (23):

$$c_1 = 0.9 \times 10^{-6} \text{ s} \quad (15)$$

$$c_2 = a/3.1 \text{ s}^2$$

The coefficients depend on the number of preamplifier circuits.

11.3.4 Standard error propagation formulae apply to estimate the random uncertainty from counting statistics.

11.4 Determine m_{eff} from the measured quantities using one of the following methods (24):

11.4.1 For the non-multiplying example in accordance with 9.4.3.1:

$$m_{eff} = (R_c - a_0)/a_1 \quad (16)$$

11.4.2 From the calibration fit in accordance with 9.4.3.2 for count rates uncorrected for neutron multiplication, the corrected reals count rate is given by:

$$R_c = a_0 + a_1 m_{eff} + a_2 (m_{eff})^2 \quad (17)$$

Inverting this equation yields the ^{240}Pu effective mass:

$$m_{eff} = \frac{-a_1 + \sqrt{a_1^2 - 4a_2(a_0 - R_c)}}{2a_2} \quad (18)$$

11.4.3 Other analysis procedures have been validated and documented. Details of these topics are beyond the scope of this test method. General information is included in Appendix X2 for reference.

11.5 The standard equation for calculating the ^{240}Pu effective mass is a function containing nuclear constants for the even-mass plutonium isotopes and is specific to the coincidence circuitry (4,11). The following equation from Reference 11 is one of the more commonly seen formulations of the m_{eff} equation.

$$m_{eff} = 2.52m_{238} + m_{240} + 1.68m_{242} \quad (19)$$

where:

m_A = known mass of plutonium Isotope A in the material.

11.6 The total plutonium in the scrap or waste package is determined by dividing m_{eff} by the effective ^{240}Pu fraction assigned to the package.

$$\text{Pu mass} = m_{eff} [2.52f_{238} + f_{240} + 1.68f_{242}] \quad (20)$$

where:

f_A = are the weight fractions of the plutonium Isotope A .

11.7 Error estimates for the Pu mass should include all components which cause significant effects. These generally include: counting statistics, calibration errors (including reference material uncertainties), matrix uncertainties, sample and nuclear material heterogeneities, and uncertainties in the isotopic ratios. Some components may be difficult to quantify. The random error standard deviation, σ_m , associated with the Pu

mass and due solely to counting statistics can be derived from the measured counting statistics by standard error propagation methods (22). This value is usually computed and printed along with the plutonium mass measurement.

12. Precision and Bias

NOTE 4—The precision and bias of passive neutron coincidence measurements are functions of several interrelated factors; consequently, a simple precision or bias statement is rarely possible. The interrelated factors include facility specific procedures, the quality of the scrap/waste segregation program, the appropriateness of the reference material matrix models, matrix types, chemical forms, and quantities. This section provides information on the topic, but cannot substitute for critical thinking, professional skill, and verification measurements. The evaluation of the uncertainty for a passive neutron coincidence measurement is not a purely mathematical task; it requires detailed knowledge of the measurement method, the procedures, and the items being measured. Measurements of uncharacterized scrap and waste items can yield results of indeterminate bias. However, a combination of measurement methods applied to such items may be used to estimate the validity of the measurements. Except for measurements of small quantities, the possibility of bias is of greater concern than the issue of inadequate precision.

12.1 The precision of a passive neutron coincidence measurement can be estimated from replicate measurements. When passive neutron coincidence counters are set up and functioning properly, they follow a Poisson distribution (9). In cases where the Poisson assumption is valid, the precision may also be estimated using statistical calculations on data from a single measurement, such as that presented in Tables 1 and 2 (25).

12.1.1 The instrument calculated values of % σ_m (σ_m expressed as a percent) given in Table 3 are examples of the counting statistics precision that can be achieved with well-characterized material. Counting statistics contribute a random error of less than 1 % of the measured mass for 300-s measurements of items containing between 10g and 150g of high purity $^{240}\text{PuO}_2$. Table 1 indicates that, for pure and impure materials containing 0.6g of effective ^{240}Pu , σ_m ranges from 2.3 % to 11.7 % for 300-s measurements (25).

12.1.2 The repeatability and reproducibility of a passive neutron coincidence measurement can be estimated from replicate measurements. For a wide variety of measurements similar to those in Tables 3 and 1, σ_m approximately estimates the standard deviation that would be observed in a series of repeated measurements.

TABLE 1 Precision Data for Passive Neutron Coincidence Counter Measurements of Plutonium with Assorted Impurities

NOTE 1—Measurement data from a set of 10 g plutonium disks (0.6 g effective ^{240}Pu) with assorted impurities (25). Measurement time was 300 s. % σ_m was calculated from the counting statistics of a single measurement and has been verified by replicate measurements.

Item ID	Material	% σ_m
A1-86	PuO ₂	3.0
A1-87	PuO ₂ + A1	5.7
A1-88	PuO ₂ + MgO	6.9
A1-89	PuO ₂ + Si	3.4
A1-90	PuO ₂ + B	11.7
A1-91	PuF ₄	7.5
A1-92	Pu Metal	2.3

TABLE 2 Bias Resulting from Passive Neutron Coincidence Counter Measurements of Plutonium Oxide

NOTE 1—Passive neutron coincidence counter measurement data for pure and slightly impure plutonium oxides (25). All measurement times were 300 s. Calibration parameters for these measurements were determined from pure PuO₂ reference materials. The % Relative Difference is the difference between the measured and reference values expressed as a percent, σ_m is 0.8 %, or better, for these measurements.

Item ID	Reference Total Pu Mass (g Pu)	Reference Effective ^{240}Pu Mass (g)	% Relative Difference
<i>Pure Plutonium Oxide</i>			
LAO261C10	847.1	144.4	0.42
LAO255C10	542.9	92.26	-0.56
LAO252C10	321.3	54.37	-2.40
<i>Impure Plutonium Oxide</i>			
PEO381	613.4	65.02	-3.71
PEO382D	299.3	29.70	-3.81

TABLE 3 Precision Data for Passive Neutron Coincidence Counter Measurements of Well Characterized Material

NOTE 1—Passive neutron coincidence counter precision data from a set of pure PuO₂ samples (25). The count time was 300 s for these measurements. % σ_m , determined from the counting statistics of a single measurement, was less than 1.0 % for each of the items.

Item ID	Reference Total Pu Mass (g Pu)	Reference Effective ^{240}Pu Mass (g)	% σ_m
LAO250C10	59.87	10.10	0.94
LAO251C10	171.6	29.29	0.82
LAO252C10	321.3	54.37	0.74
LAO256C10	384.2	65.15	0.72
LAO255C10	542.9	92.26	0.70
LAO253C10	611.7	104.6	0.6
LAO261C10	847.1	144.4	0.65
LAO261C11	875.0	149.2	0.64

12.1.3 In general, longer counting times, larger quantities of nuclear material, and use of instruments with higher detection efficiencies will improve measurement precision.

12.1.4 Precision and bias are dependent upon many factors relating to the segregation and packaging of materials, as well as the physical and chemical form of the plutonium. For example, bias introduced by matrix differences can be minimized by a waste and scrap segregation plan and may be detected by monitoring changes in the ratio R/T. Also, if the characteristics of the material do not match the materials used in the calibration, the bias may increase indeterminately. Table 2 illustrates the percent relative difference between the measured and reference effective ^{240}Pu masses for pure and slightly impure plutonium oxides.

12.2 Each user of this test method should determine the precision and bias for their specific scrap and waste categories (26).

12.2.1 In addition to the checks described in 9.3, a comparison of the results with another assay technique (such as segmented gamma-ray scanning, calorimetry, or destructive analysis) can be quite helpful. In general, two techniques based on different physical properties are susceptible to different sources of bias (27,28).

12.2.2 Figs. 4 and 5 compare the results of passive neutron coincidence measurements with results derived from alternative techniques. Fig. 4 compares passive neutron measurements with segmented gamma scanner measurements (ASTM C 1133) for 19 liter 5 gallon pails containing plutonium scrap (29). Fig. 5 compares passive neutron measurements with calorimetry (30). These matrices do not contain large amounts of hydrogen and were generated at two different plutonium processing facilities. Both Figs. 4 and 5 suggest that an individual passive neutron coincidence counter measurement may be biased as much as 10 % to 20 % compared to the other method.

12.3 This technique measures the abundances of the even isotopes of plutonium. Biases in the determination of the relative abundances of the isotopes of plutonium will result in significant bias in the calculated total mass of plutonium. A fractional bias in m_{eff} propagates to the same fractional bias in the total plutonium mass.

12.4 Reference materials are assigned plutonium mass and isotopic ratio values which have uncertainties associated with them. Calibrations are based on these “known” values. If there are biases in the “known” values of the reference materials, they will cause a bias in the neutron assay. Uncertainties in “known” values must be propagated into the calculated uncertainty of an assay.

12.5 Cosmic-ray background can be significant for small plutonium loadings in the presence of large quantities of high atomic number matrix. The bias effect is of the order of 0.02 g m_{eff} at sea level, and can double at high elevation (2000 m) (19).

12.6 If the detection efficiency is not constant over the assay volume, bias effects can occur due to sample positioning or varying fill heights of the material in the container. The detection efficiency of some 208 1 systems has been determined to vary as much as 15 % for the totals and 28 % for coincidence count rates over the volume of the assay chamber (4, 8, 19, 27).

12.7 Neutron multiplication effects increase with plutonium mass, and are affected by geometrical variations in the distri-

bution of the plutonium and the presence of moderating and (α, n) producing materials.

12.7.1 The nonlinearity of the uncorrected PuO₂ calibration curve in Fig. 3 is attributable to neutron multiplication.

12.7.2 Neutrons from (α, n) reactions in low atomic number matrices can induce fissions also. This will bias the result high unless the multiplication correction technique is used. (See Appendix X2.)

12.7.3 Multiplication effects are larger for counting chambers without a cadmium liner.

12.8 The hydrogen content (water, plastic, acid, etc.) of an assay item may increase the detection efficiency and multiplication effects by lowering the average neutron energy, thereby causing a bias. The largest potential inaccuracies associated with nonuniform source distributions in passive neutron coincidence counters is found when large amounts of moderating material are contained in the scrap or waste matrix. Average to minimum passive response ratios of 4.5 have been reported for highly moderating matrices with hydrogen densities above 0.04 g/cm³ (31). In severe cases where the hydrogen content varies unexpectedly from the reference materials used for calibration, the effect can cause the plutonium mass result to double for 50 g m_{eff} (32).

12.9 Sample container wall effects, for example, polyethylene liners, have biased individual assay results as much as 7 %. It is important to standardize waste containers, preferably using materials which do not absorb or moderate neutrons.

12.10 Measurements of plutonium items with uranium contamination will be biased unless corrections are made (33).

12.11 According to a recent experiment (34), the presence of neutron absorbers in the matrix does not cause a bias in passive neutron coincidence measurements. No bias is introduced because only thermal neutrons are absorbed by neutron absorbing materials. And a change in the number of thermal neutrons will not affect the coincidence count rate because these neutrons 1) move too slowly to appear in coincidence or, 2) do not pass through the cadmium liner or 0.5" to 1.0" of polyethylene present in most passive neutron coincidence counters.

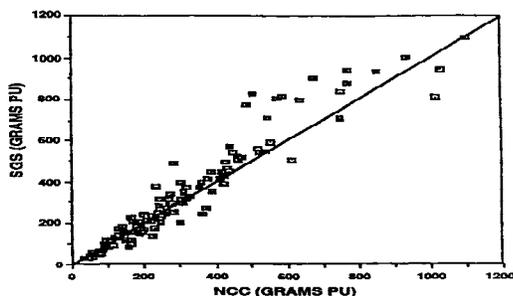
12.12 Mixing other spontaneous fission isotopes with the plutonium will increase R . These materials must be segregated and assayed by another method, unless a correction is made in the m_{eff} formula. Curium has been a problem in high burn-up plutonium.

12.13 The density of the plutonium compound can have significant effects on R . An increase in the plutonium density increases the sample multiplication. R can vary as much as 10 % for a can of oxide if the can is tumbled several times to fluff up the powder (30).

12.14 The instability of modern electrical circuits contributes a negligible error (<0.1 %) to the results (35). Proper adjustment of parameters such as the pre-delay and the gate length cause their potential for bias effects to become negligible.

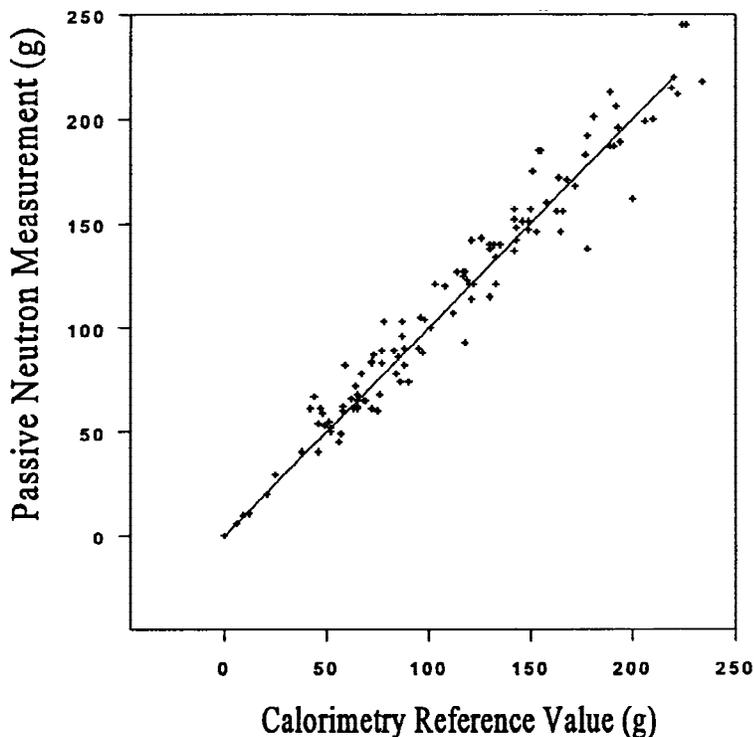
13. Keywords

13.1 nondestructive assay; passive neutron coincidence counting; plutonium; scrap and waste



NOTE 1—The results of passive neutron coincidence measurements of the plutonium content of 5-gal. pails are compared to the results of Segmented Gamma Scanner (SGS) measurements. The pails contain scrap and waste generated by a plutonium reprocessing facility in Aiken, South Carolina (28). The matrices have no hydrogen. The measurement uncertainties for both techniques are dominated by bias rather than precision.

FIG. 4 Comparison of Neutron Coincidence Counter Measurements of Plutonium with SGS Measurements



NOTE 1—The results of passive measurements of the plutonium content of small containers of scrap and waste are compared to the results of calorimetry and gamma-ray isotopic measurements. The containers were generated at a plutonium R&D facility in Los Alamos. The matrices do not contain hydrogen. The measurement uncertainties are dominated by bias rather than precision.

FIG. 5 Comparison of Neutron Coincidence Counter Measurements of Plutonium with Results Obtained from Calorimetry and Gamma-Ray Isotopics Analysis

APPENDIXES

(Nonmandatory Information)

X1. Use of the R/T Ratio for Evaluating Assay Results

X1.1 Some applications have used the reals-to-totals ratio, R/T , to help evaluate the suitability of the selected calibration curve (27). The following information is presented here to help the potential user, primarily because it is not yet widely documented in the technical literature.

X1.1.1 For the particular case of the high-level neutron coincidence counter, (HLNCC), non-multiplying plutonium metal has an R/T ratio of approximately 0.1. For ^{252}Cf the R/T ratio is approximately 0.18; for non-multiplying plutonium

oxide, the R/T ratio ranges from 0.04 to 0.08. With increasing (α, n) contribution, these ratios get much smaller.

X1.1.2 As the R/T ratio approaches zero, it indicates that fewer of the neutrons are from fission events. In this case, the induced fission rate in ^{239}Pu may become a significant portion of the total fission rate. The usual consequence of this is that the assay result is biased high. The selected calibration curve may not be suitable and alternative analysis methods are needed (27).

X2. Methods for Treating Neutron Multiplication of Well-Characterized Material

X2.1 The following information is included to show methods which have been applied to well-characterized material in which there is known neutron multiplication or for the case where there is little neutron count rate.

X2.1.1 *Known Multiplication Method* (3)—For similar geometries and plutonium loadings the neutron multiplication M is assumed to be related to the ^{239}Pu mass. M is obtained from

the reference materials or Monte Carlo calculations, while the measured quantities R_c and T_c are used to solve for the (α, n) component and m_{eff} .

X2.1.2 *Multiplication Corrected Reals* R_{MC} (3, 34)—Compute the (α, n) effects from the known chemical composition. Compute M , then use R_c , and M to compute R_{MC} . A linear relationship should exist between R_{MC} and m_{eff} . When the

chemical composition of the plutonium is known, this approach gives the most accurate results for the widest range of material categories with a single calibration.

X2.1.3 *Self-Interrogation Method* (26)—This technique requires the induced fission response to be comparable to or larger than the spontaneous fission response.

X3. Comparison of the $r + a$ and τ Registers

X3.1 A feature of the shift register coincidence circuit is that the $r+a$ coincidence sum can exceed the totals τ during a measurement. This could come about, for example, if four neutrons are detected within one coincidence gate width. Then the totals will be incremented by four while $r+a$ increments by six. The first neutron starts a coincidence gate and it counts the three subsequent neutrons. The second neutron starts a second coincidence gate, and it counts the two subsequent neutrons.

X2.1.4 For very small plutonium loadings, a more sensitive upper limit determination of the amount of plutonium in the sample may be achieved from relating m_{eff} to the totals count rate T for R in Eq 18. The totals count rate is more susceptible to background and matrix effects than is the real count rate R .

The third neutron starts another coincidence gate, and it counts the last neutron. The last neutron starts a coincidence gate that counts no neutrons in the $r+a$ scaler. In this example, the sum of the six $r+a$ coincidence events exceeds the four neutrons detected in the totals scaler. When the $r+a$ sum exceeds the totals sum, the operator should not assume that the shift register has malfunctioned or that the data are invalid.

REFERENCES

- (1) Menlove, H.O., Baca, J., Harker, W., Kroncke, K.E., Miller, M.C., Takahashi, S., Kobayashi, H., Seki, S., Matsuyama, K., Kobayashi, S., "WDAS Operation Manual Including the Add-A-Source Function", Los Alamos National Laboratory Report LA-12292-M, Los Alamos, NM, 1992.
- (2) Menlove, H. O. and Stewart, J. E., "A New Method of Calibration and Normalization for Neutron Detector Families", Los Alamos Report LA-11229-MS, 1988.
- (3) Menlove, H. O., Abedin-Zadeh, R., Zhu, R., "The Analysis of Neutron Coincidence Data to Verify Both Spontaneous-Fission and Fissionable Isotopes", Los Alamos Report LA-11639-MS, 1989.
- (4) Böhnel, K., "Die Plutoniumbestimmung in Kernbrennstoffen mit der Neutronen Koinzidenzmethode", Karlsruhe Report KRK2203, 1975; A WRE translation No. 70 (54/4252), 1978.
- (5) Dytlewski, N., Ensslin, N., Boldeman, J. W., "A Neutron Multiplicity Counter for Plutonium Assay", *Nucl. Sci. and Eng.* 104, 301-313, 1990.
- (6) Hage, W. and Cifarelli, D. M., "On the Factorial Moments of the Neutron Multiplicity Distribution of Fission Cascades", *Nucl. Instr. and Meth. in Phys. Res. A*, 236, 165-177, 1985.
- (7) Menlove, H. O., Foster, L. A., Baca, J., "NBC Operation Manual Including the Multi-Position Add-A-Source Function", Los Alamos Report LA-12737-M, 1994.
- (8) Miller, D. W. and Menlove, H.O., "Cosmic-Ray-Veto Detector System", Los Alamos Report LA-12469-MS, 1992.
- (9) Krick, M. S. and Menlove, H. O., "The High-Level Neutron Coincidence Counter (HLNCC) User's Manual", Los Alamos Report LA 7779-M, 1979.
- (10) Swansen, J. and Collingsworth, P., "High-Level Coincidence Counter Maintenance", Los Alamos Report LA 9662-M, 1983.
- (11) Krick, M. S., "²⁴⁰Pu-effective Mass Formula for Coincidence Counting of Plutonium with SR Electronics", Los Alamos Report LA-7030-PR, 1977.
- (12) US DOE Order 5820.2, "Waste Management", U.S. Department of Energy, Washington DC, Sep 26, 1988, Definition 39.
- (13) US DOE Order 5633.3, "Control and Accountability of Nuclear Material", U.S. Department of Energy, Washington, DC, February 3, 1988, Paragraph II.3 and II.5
- (14) Goldman, A. and DeRidder, P., "Calibration Functions for PFPF Neutron Coincidence Data", EDE-241/88, MA-JPN-33 1988.
- (15) Knief, R. A., "Nuclear Energy Technology - Theory and Practice of Commercial Nuclear Power", McGraw-Hill Book Company (revised 1989) Chapter 4.
- (16) Miller, D.W. and Ensslin, N., "Drum Counter Design and Operation Manual", Los Alamos National Laboratory Report LA-11892-M, Los Alamos, NM, 1990.
- (17) Menlove, H.O. and Eccleston, G.W., "High Sensitivity Measurements for Low-Level TRU Wastes Using Advanced Passive Neutron Techniques, Los Alamos National Laboratory Report LA-UR-92-2563, 1992.
- (18) Knoll, G. F., "Radiation Detection and Measurement", Second Edition, John Wiley & Sons, 1989.
- (19) Ensslin, N., "Principles of Neutron Coincidence Counting" in *Passive Nondestructive Assay of Nuclear Materials*, T.D. Reilly, H.A. Smith, Jr., N. Ensslin, and S. Kreiner, eds, NRC Report NUREG/CR 550, March, 1991.
- (20) Menlove, H.O., and Swansen, J.E., "A High-Performance Neutron Time Correlation Counter", *Nucl. Tech.*, Vol. 71, 1985.
- (21) Hsue, S. -T., Campbell, K., Barlich, G., "Measurement Control Program for New Special Recovery", Los Alamos Report LA-10974-MS, 1987.
- (22) Dytlewski, N., Krick, M. S., Ensslin, N., "Measurement Variances in Thermal Neutron Coincidence Counting", *Nucl. Instr. Meth.* A327, 469-479, 1993.
- (23) Swansen, J. E., "Deadtime Reduction in the High Level Neutron Coincidence Counter HLNCC", Los Alamos Report LA-9936-MS, 1984.
- (24) Bevington, P. R., "Data Reduction and Error Analysis for the Physical Sciences", McGraw-Hill Inc., 1969.
- (25) Private communication between James Sprinkle of the Los Alamos National Laboratory Safeguards Science and Technology Group and Dr. Joseph Wachter.
- (26) Hooten, B. W. and Rogers, F. J., "Calibration of Passive Neutron Coincidence Counters and an Assessment of Overall Errors", NMACT, 1984, p.26, United Kingdom Atomic Energy Authority, NMACT.AERE Harwell, England.
- (27) Hsue, S. -T., Langner, D. G., Longmire, V. L., Menlove, H. O., Russo, P. A., Sprinkle Jr., J. K., "Measurements of Plutonium Residues from Recovery Processes", Los Alamos Report LA-UR-89-3699 presented at The Topical Meeting on Waste Measurements, Cadarache, France, November 1989.

- (28) Sprinkle Jr., J. K., Bosler, G. E., Hsue, S. -T., Kellogg, M. P., Miller, M. C., Simmonds, S. M., and Smith, A. R., “Nondestructive Assay of Plutonium-Bearing Scrap and Waste”, Los Alamos Report LA-UR-89-2373 presented at the ANS meeting in San Francisco, November 1989.
- (29) Baker, M., MacMurdo, K., Miller, M. C., Bosler, G. E., “Recent Experiences of Scrap and Waste Assay Using Neutron Coincidence Counting of Materials from F-B Line at the Savannah River Site”, Proc. of the XXXI Institute of Nuclear Materials Management Meeting, Los Angeles, July 1990.
- (30) Wachter, J. R., Maez, R., Foster, L. A., Pompeo, J. “Non Destructive Measurement Uncertainty at a Plutonium Scrap Recovery Facility”, Proc. of XXXVI Institute of Nuclear Materials Management Meeting, Palm Desert, CA, July 1995.
- (31) Rinard, P. M., Adams, E. L., Menlove, H. O., Sprinkle Jr., J. K., “Characterizing and Improving Passive-Active Shufflers for Assays of 208-Liter Waste Drums”, 14th ANNUAL ESARDA MEETING, Salamanca, Spain, May 5-8, 1992.
- (32) Crane, T. W., “ Calibration of a Neutron Coincidence Counter for Measurement of the Plutonium Content of Wet Oxalate Cakes”, Los Alamos Report LA-9744-MS, 1983.
- (33) Ensslin, N., “A Simple Self-Multiplication Correction for In-Plant Use”, 7th ESARDA SYMPOSIUM on Safeguards on Safeguards and Nuclear Material management, Liege, Belgium, May 21-23, 1985.
- (34) Personal correspondence from Dr. Phillip Rinard to Dr. Joseph Wachter dated June 27, 1996.
- (35) Goldman, A., Auguston, R., and Karlin, E. W., “A Humidity Temperature Test on the HLNCC Instrument, Los Alamos Report LA-UR-87-2254, 1987.

ASTM International takes no position respecting the validity of any patent rights asserted in connection with any item mentioned in this standard. Users of this standard are expressly advised that determination of the validity of any such patent rights, and the risk of infringement of such rights, are entirely their own responsibility.

This standard is subject to revision at any time by the responsible technical committee and must be reviewed every five years and if not revised, either reapproved or withdrawn. Your comments are invited either for revision of this standard or for additional standards and should be addressed to ASTM International Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee, which you may attend. If you feel that your comments have not received a fair hearing you should make your views known to the ASTM Committee on Standards, at the address shown below.

This standard is copyrighted by ASTM International, 100 Barr Harbor Drive, PO Box C700, West Conshohocken, PA 19428-2959, United States. Individual reprints (single or multiple copies) of this standard may be obtained by contacting ASTM at the above address or at 610-832-9585 (phone), 610-832-9555 (fax), or service@astm.org (e-mail); or through the ASTM website (www.astm.org).